

Jednačine telegrafičara za idealan vod

$$\underline{U}_2 = \underline{U}_1 \cos \beta L - j Z_c \underline{I}_1 \sin \beta L \quad \underline{I}_2 = \underline{I}_1 \cos \beta L - j \frac{\underline{U}_1}{Z_c} \sin \beta L$$

Parametri pojedinačnih namotaja tronamotajnog transformatora

$$R_1 = \frac{1}{2}(R_{12} + R_{13} - R_{23}) \quad R_2 = \frac{1}{2}(R_{12} + R_{23} - R_{13}),$$

$$R_3 = \frac{1}{2}(R_{13} + R_{23} - R_{12})$$

Parametri nesimetrične π šeme regulacionog transformatora

$$\underline{Z}_1 = \frac{t^2 \underline{Z}_T}{1-t} \quad \underline{Z}_2 = t \underline{Z}_T \quad \underline{Z}_3 = \frac{t \underline{Z}_T}{t-1}$$

Formule za padove napona

$$\underline{U}_1 = \underline{U}_2 + \frac{P_2 R + Q_2 X}{U_2} + j \frac{P_2 X - Q_2 R}{U_2}$$

$$\underline{U}_2 = \underline{U}_1 - \frac{P_1 R + Q_1 X}{U_1} - j \frac{P_1 X - Q_1 R}{U_1}$$

$$\underline{U}_2 = \frac{\underline{U}_1}{2} + \sqrt{\left(\frac{\underline{U}_1}{2}\right)^2 - P_2 R - Q_2 X - \left(\frac{P_2 X - Q_2 R}{U_1}\right)^2} - j \frac{P_2 X - Q_2 R}{U_1}$$

$$\underline{U}_1 = \frac{\underline{U}_2}{2} + \sqrt{\left(\frac{\underline{U}_2}{2}\right)^2 + P_1 R + Q_1 X - \left(\frac{P_1 X - Q_1 R}{U_2}\right)^2} + j \frac{P_1 X - Q_1 R}{U_2}$$

Statički koeficijenti promene snage sa promenom napona

$$P_p = C_{PU} U^{k_{PU}} \quad Q_p = C_{QU} U^{k_{QU}}$$

$$P_p = P_{po} + P_{po} k_{PU} \frac{U - U_o}{U_o} \quad Q_p = Q_{po} + Q_{po} k_{QU} \frac{U - U_o}{U_o}$$

Elementi matrice admintansi nezavisnih čvorova ($[\underline{Y}_{\check{c}v}]$)

$$\underline{Y}_{ii} = \sum_{\substack{j=0 \\ j \neq i}}^N Y_{ij}^{gr} \quad (\text{na glavnoj dijagonali}) \quad \underline{Y}_{ij} = -\underline{Y}_{ij}^{gr} \quad (\text{van dijagonale})$$

Jednačine za formiranje matrice impedansi nezavisnih čvorova ($[\underline{Z}_{\check{c}v}]$)

a) Novi čvor (k) - referentni čvor (o) - grana \underline{Z}_{ko}^{gr}

$$[\underline{Z}_{\check{c}v}]^{post} = \left[\begin{array}{c|c} [\underline{Z}_{\check{c}v}]^{pre} & \begin{matrix} 0 \\ \vdots \\ 0 \end{matrix} \\ \hline 0 \quad \dots \quad 0 & \underline{Z}_{ko}^{gr} \end{array} \right]$$

b) Novi čvor (k) - stari čvor (j) - grana \underline{Z}_{kj}^{gr}

$$[\underline{Z}_{\check{c}v}]^{post} = \left[\begin{array}{c|c} [\underline{Z}_{\check{c}v}]^{pre} & \begin{matrix} \underline{Z}_{1j} \\ \vdots \\ \underline{Z}_{n^o j} \end{matrix} \\ \hline \underline{Z}_{j1} \quad \dots \quad \underline{Z}_{jn^o} & \underline{Z}_{jj} + \underline{Z}_{kj}^{gr} \end{array} \right], \quad n^o \text{ je dimenzija } [\underline{Z}_{\check{c}v}]^{pre}$$

c) Stari čvor (j) - referentni čvor (o) - grana \underline{Z}_{jo}^{gr}

$$[\underline{Z}_{\check{c}v}]^{post} = [\underline{Z}_{\check{c}v}]^{pre} - [\Delta \underline{Z}_{\check{c}v}]$$

$$[\Delta \underline{Z}_{\check{c}v}] = \frac{1}{\underline{Z}_{jj} + \underline{Z}_{jo}^{gr}} \begin{bmatrix} \underline{Z}_{1j} \\ \vdots \\ \underline{Z}_{n^o j} \end{bmatrix} \begin{bmatrix} \underline{Z}_{j1} & \dots & \underline{Z}_{jn^o} \end{bmatrix}, \quad n^o \text{ je dimenzija } [\underline{Z}_{\check{c}v}]^{pre}$$

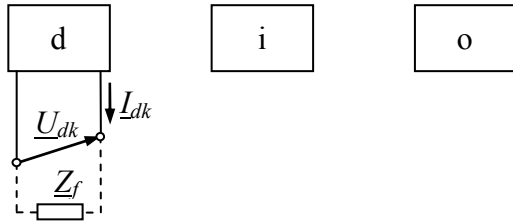
d) Stari čvor (i) - stari čvor (j) - grana \underline{Z}_{ij}^{gr}

$$[\underline{Z}_{\check{c}v}]^{post} = [\underline{Z}_{\check{c}v}]^{pre} - [\Delta \underline{Z}_{\check{c}v}]$$

$$[\Delta \underline{Z}_{\check{c}v}] = \frac{1}{\underline{Z}_{ii} + \underline{Z}_{jj} - 2\underline{Z}_{ij} + \underline{Z}_{ij}^{gr}} \begin{bmatrix} \underline{Z}_{1i} - \underline{Z}_{1j} \\ \vdots \\ \underline{Z}_{n^o i} - \underline{Z}_{n^o j} \end{bmatrix} \begin{bmatrix} (\underline{Z}_{i1} - \underline{Z}_{j1}) & \dots & (\underline{Z}_{in^o} - \underline{Z}_{jn^o}) \end{bmatrix}$$

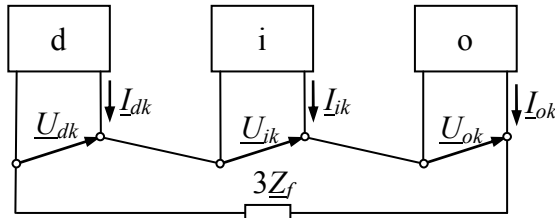
Proračun kratkih spojeva matricnom metodom

a) Trofazni kratki spoj (3kz)



$$\underline{I}_{dk} = \frac{\underline{E}}{\underline{Z}_{(k,k)}^d + \underline{Z}_f}, \quad \underline{U}_{dl} = \underline{E} - \underline{Z}_{(l,k)}^d \underline{I}_{dk}, \quad l = 1, \dots, n$$

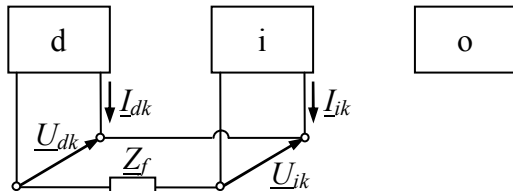
b) Jednofazni kratki spoj (1kz)



$$\underline{I}_{dk} = \underline{I}_{ik} = \underline{I}_{ok} = \frac{\underline{E}}{\underline{Z}_{(k,k)}^d + \underline{Z}_{(k,k)}^i + \underline{Z}_{(k,k)}^o + 3\underline{Z}_f}$$

$$\underline{U}_{dl} = \underline{E} - \underline{Z}_{(l,k)}^d \underline{I}_{dk}, \quad \underline{U}_{il} = -\underline{Z}_{(l,k)}^i \underline{I}_{ik}, \quad \underline{U}_{ol} = -\underline{Z}_{(l,k)}^o \underline{I}_{ok}, \quad l = 1, \dots, n$$

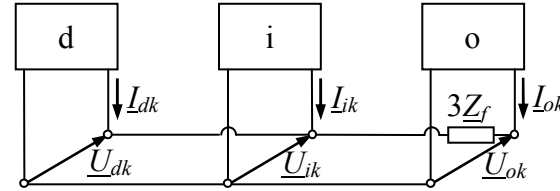
c) Dvofazni kratki spoj bez zemlje (2k)



$$\underline{I}_{dk} = -\underline{I}_{ik} = \frac{\underline{E}}{\underline{Z}_{(k,k)}^d + \underline{Z}_{(k,k)}^i + \underline{Z}_f}, \quad \underline{I}_{ok} = 0$$

$$\underline{U}_{dl} = \underline{E} - \underline{Z}_{(l,k)}^d \underline{I}_{dk}, \quad \underline{U}_{il} = -\underline{Z}_{(l,k)}^i \underline{I}_{ik}, \quad \underline{U}_{ol} = 0, \quad l = 1, \dots, n$$

d) Dvofazni kratki spoj sa zemljom (2kz)



$$\Delta = \underline{Z}_{(k,k)}^d (\underline{Z}_{(k,k)}^i + \underline{Z}_{(k,k)}^o + 3\underline{Z}_f) + \underline{Z}_{(k,k)}^i (\underline{Z}_{(k,k)}^o + 3\underline{Z}_f)$$

$$\underline{I}_{dk} = \frac{\underline{E} (\underline{Z}_{(k,k)}^i + \underline{Z}_{(k,k)}^o + 3\underline{Z}_f)}{\Delta}$$

$$\underline{I}_{ik} = -\frac{\underline{E} (\underline{Z}_{(k,k)}^o + 3\underline{Z}_f)}{\Delta}, \quad \underline{I}_{ok} = -\frac{\underline{E} \underline{Z}_{(k,k)}^i}{\Delta}$$

$$\underline{U}_{dl} = \underline{E} - \underline{Z}_{(l,k)}^d \underline{I}_{dk}, \quad \underline{U}_{il} = -\underline{Z}_{(l,k)}^i \underline{I}_{ik}, \quad \underline{U}_{ol} = -\underline{Z}_{(l,k)}^o \underline{I}_{ok}, \quad l = 1, \dots, n$$

Simetrične komponente struje po grani k-l

$$\underline{I}_{kl}^{(d,i,o)} = \frac{\underline{U}_k^{(d,i,o)} - \underline{U}_l^{(d,i,o)}}{\underline{Z}_{kl}^{gr(d,i,o)}}$$

Transformacija simetričnih komponenata u fazne i obratno

$$\begin{bmatrix} \underline{I}_a \\ \underline{I}_b \\ \underline{I}_c \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ 1 & \underline{a}^2 & \underline{a} \\ 1 & \underline{a} & \underline{a}^2 \end{bmatrix} \begin{bmatrix} \underline{I}_o \\ \underline{I}_d \\ \underline{I}_i \end{bmatrix}, \quad \begin{bmatrix} \underline{I}_o \\ \underline{I}_d \\ \underline{I}_i \end{bmatrix} = \frac{1}{3} \begin{bmatrix} 1 & 1 & 1 \\ 1 & \underline{a} & \underline{a}^2 \\ 1 & \underline{a}^2 & \underline{a} \end{bmatrix} \begin{bmatrix} \underline{I}_a \\ \underline{I}_b \\ \underline{I}_c \end{bmatrix}$$

Uticao na TK vod

$$E = 3|\underline{I}_o| \cdot 2\pi f \cdot L_p \cdot k_z \frac{4}{\sqrt{a}}$$

U slučaju kose deonice TK voda, rastojanje a se računa kao geometrijska sredina dva krajnja rastojanja a_1 i a_2 , odnosno $a = \sqrt{a_1 a_2}$.